

ANALYSIS OF RING JET LASER GYRO RESONANT DITHERING MECHANISM

Penumarthi Chandra Sekhar Kumar¹, Bharatam Anil Kumar²,
Marella Sai Chandra Sekhar³

¹Student, ²Assistant Professor,

Department of Mechanical Engineering,

Kallam Harinathreddy Institute of Technology, Chowdavaram, Guntur, India

³Assistant Professor, Department of Mechanical Engineering,

KKR & KSR Institute of technology and science, Vinjanampadu, Guntur, India

ABSTRACT

This paper presents the design, manufacture, testing and improvement of newly developed piezoelectric torsion actuator which generates angular displacement using piezo ceramics and torsion bar. The proposed piezoelectric torsion actuator generates angular displacement during dithering, directly invoking the shear mode of the piezoelectric material and hence no complicated additional mechanism is needed. The piezo plates are formed from a rectangular PZT material duly poled along the axial direction. The dither mechanism is divided into four segments that are arranged in circular configuration. Each of the segments of our piezoplates is bonded in opposite poling directions with soldering adhesive. The key to design of such an actuator is to match the torsion resonant frequency of the actuator with the excitation frequency. FEA for the Torsion bar is carried out to find the different resonant mode and mode shapes. Also, a set of torsion bars and resonator are analyzed to evaluate the maximum angular displacement and stresses on torsion bars. An experimental investigation in terms of electrical impedance and angular displacement measurement was conducted to verify the mode analysis. Based on the FEA analysis, a new material for the torsion actuator was selected having high Curie temperature and stable relative dielectric constant so that it has higher sensitivity even after bonding the piezo plates on torsion bars and also wire soldering process. The design analysis was verified with the experimental results for incorporation of the selected mechanism for the production of dither in the system.

KEYWORDS: Dithering Mechanism, Ring jet Analysis, Gyro resonant dithering mechanism, Gyro resonant mechanism

I. INTRODUCTION

Torsion bars are very important sub-assembly for gyro functioning. During very low rate of rotation, gyro does not give any output due to lock-in of CW and CCW rotating laser beam. In order to overcome this lock-in problem, an artificial rotation is being introduced for proper functioning of gyro at low rotation rates and the same rotation rate will be subtracted from the final output of gyro to get the correct rotation rate. Ring laser gyroscopes are able to detect the rotation rate of their cavity relative to an inertial frame. Their principle of operation exploits the Sagnac effect: rotation causes the length of the cavity as seen by the two counter-propagating running waves in the laser to be slightly different. In the ring laser gyroscope this difference translates directly in optical frequency shift between the two beams. Compared to conventional spinning gyroscopes, a ring laser gyro shows several advantages: they have large dynamic range, high precision, small size, they do not require any moving mechanical part and they are insensitive to translational accelerations. Laser gyros acquire a prominent role in many applications, ranging from inertial navigation system on commercial airliners, ships and spacecraft to geodesy and geophysics, to test of fundamental physics.

II. DESIGN CONCEPT

The newly developed piezo-electric torsion actuator generates angular displacement using Piezo ceramics and a torsion bar. Because of the proposed piezoelectric torsional actuator generates torsional displacement, directly invoking the shear mode of the piezoelectric material, no complicated additional mechanism is needed. The key to design such an actuator is to match the tensional resonant frequency of the actuator with its excitation frequency. Finite element analysis (FEA) of torsion bar is performed to find the torsion bar resonant modes. As a result, a maximum angular displacement of approximately 180 arc seconds was measured. A resonance decreases due to the added mass on the torsion bar is observed.

Piezo electric means having ability to generate mechanical force when electrical field is applied and vice versa. The generating mechanical force is directly proportional to the applied electric field. So that, angular rotation can be controlled by varying the electric field intensity on piezo plates.

The property of the metal that causes to produce mechanical force in terms of VIBRATIONS when voltage is applied. Here the metal is considered as the torsion bar, which produces the vibrations. Sixteen numbers of rectangular piezo plates are fixed on four torsion bars to generate dithering. Four piezo plates on each torsion bar are soldered as polarity specified in the figure (1). Polarity of piezo plates and position of soldering on flat surface of torsion bar is very important. Electrical inter connectivity is ensured for sixteen piezo plates and electric field specified frequency is applied. Contraction and expansion of piezo plate's takes place at perpendicular to the electric field applied (i.e. d31 mode). The generated forces on piezo plates are transfer to the torsion bar which deflects in the first mode of natural frequency of torsion bar shown in the figure below.

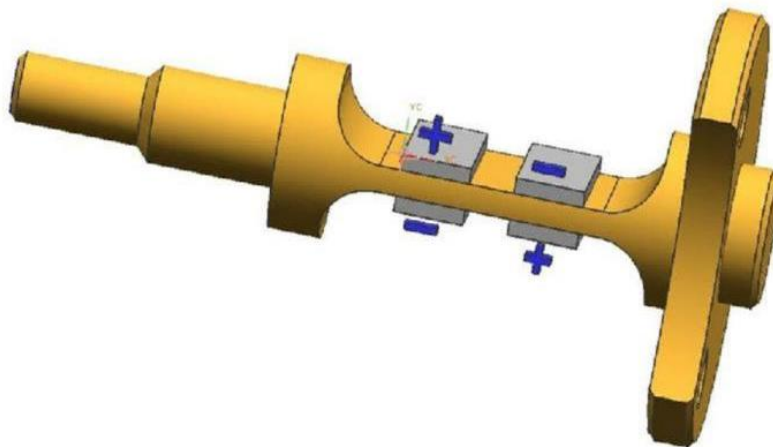


Figure 1: Piezo plates soldering on Torsion bar

The four torsion bars are vertically mounted on a single plane of a circle at 90° equally.

The vector forces shown in figure (2) indicate the applying forces on four torsion bars and its resultant orthogonal forces. So the applied force will be converted into two orthogonal forces on each torsion bar. The force diagram shows 8 orthogonal forces being generated by four applied forces. The 8 orthogonal forces are becoming four synchronized couples and resultant will be an angular rotation.

- i.e. couple1 =Orthogonal force C1 and Orthogonal force C5
- Couple2 =Orthogonal force C2 and Orthogonal force C6
- Couple3 =Orthogonal force C3 and Orthogonal force C7
- Couple4 =Orthogonal force C4and Orthogonal force C8

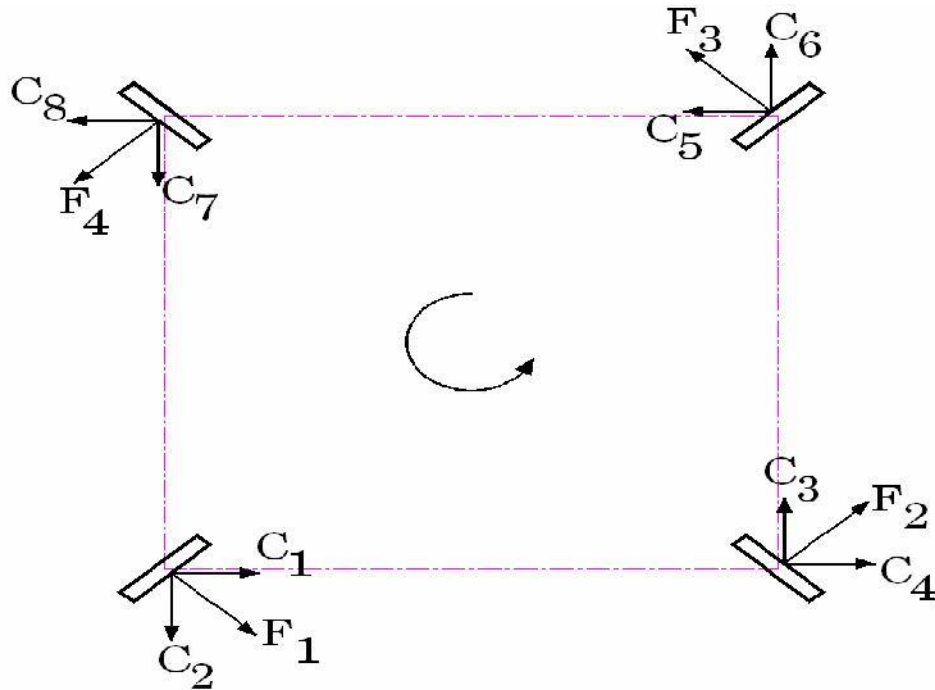


Figure 2: Coupled forces

III. MODELLING AND ANALYSIS

Selection of piezo material:

Specifications of Piezo Plate

- Dimensions : 12 X 5.5X0.35mm
- Piezo Modulus d31 : $-240 \times 10^{-12} \text{C/N}$
- Capacitance : 3000 pF
- Dielectric Loss : 0.028
- Insulation Resistance : $2 \times 10^8 \Omega$
- Electrical Strength : $1 \times 10^6 \text{V/m}$
- Operating Temperature : -60°C to $+100^\circ\text{C}$
- Voltage frequency 'f' : 400Hz

3.1 Torsion bar Material and its Mechanical Properties:

Torsion bars are made of tin free beryllium bronze material. The material properties are high strength and very good durability after temperature cycle, good spring properties, good antifricition properties, and medium electro and heat conductivity.

Mechanical properties of the torsion bar after solution annealed and precipitation- hardened condition are as follows.

1. Tensile strength = 1150- 1305 N/mm²
2. Yield strength = 1000 – 12050 N/mm²
3. Modulus of elasticity = $120 \times 10^3 \text{N/mm}^2$
4. Modulus of torsion = $47 \times 10^3 \text{N/mm}^2$
5. Hardness = 36–39HRc.

3.2 Structural Static Analysis

- Structural static analysis has been done for Torsion bar of thickness 3mm (400Hz).
- Considering the maximum force of 210N

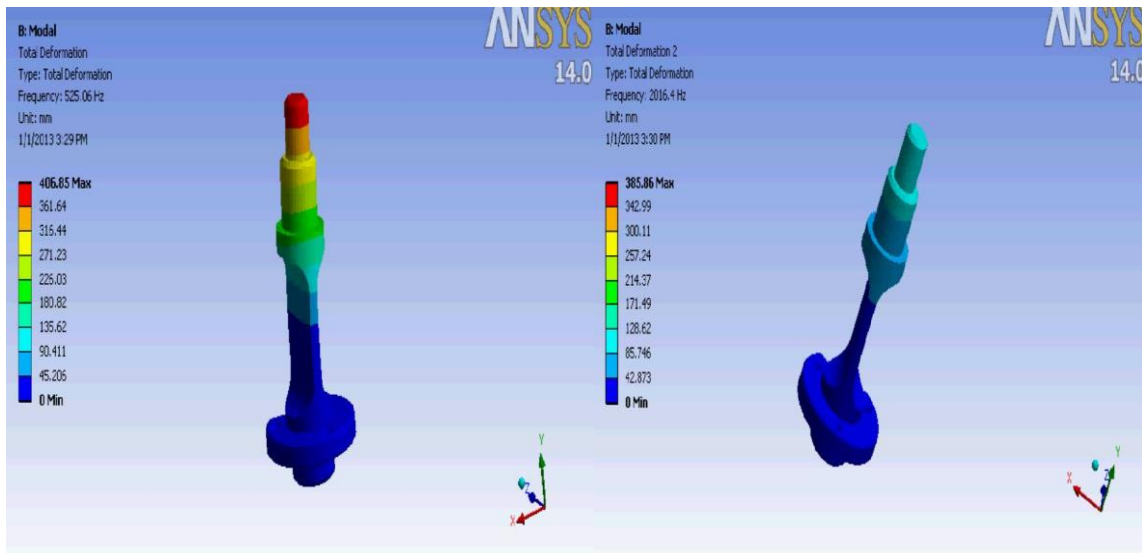


Figure 3: First mode natural frequency and mode shape

Figure 4: Second mode natural frequency and mode shape

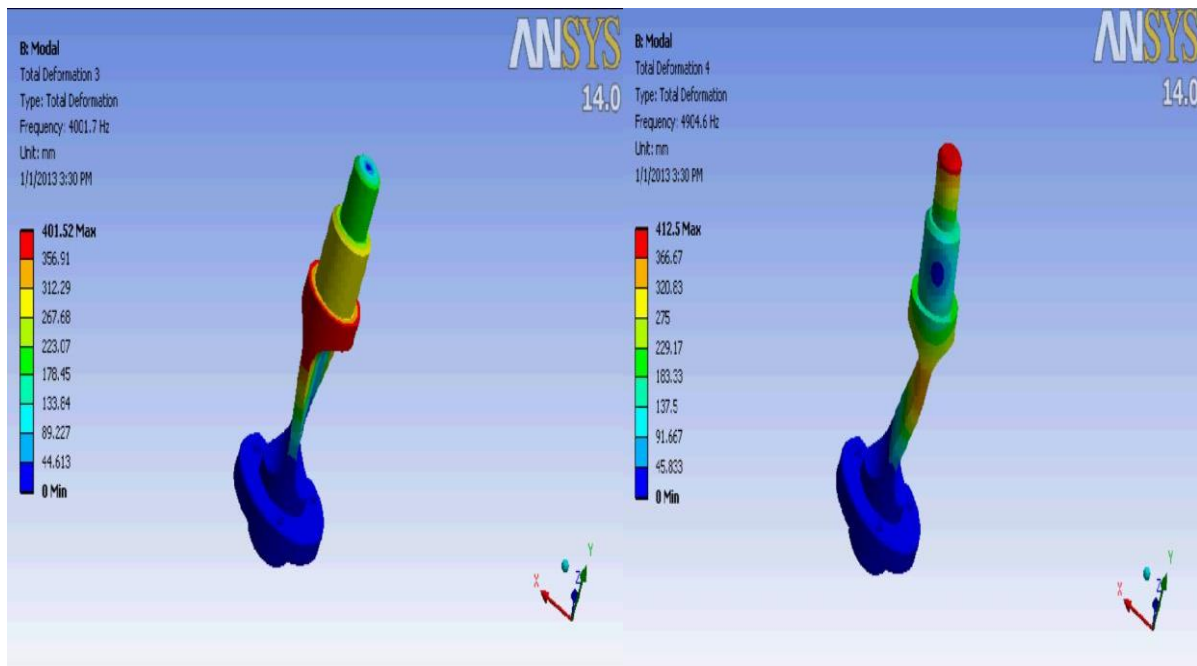


Figure 5: Third mode natural frequency and mode shape

Figure 6: Fourth mode natural frequency and mode shape

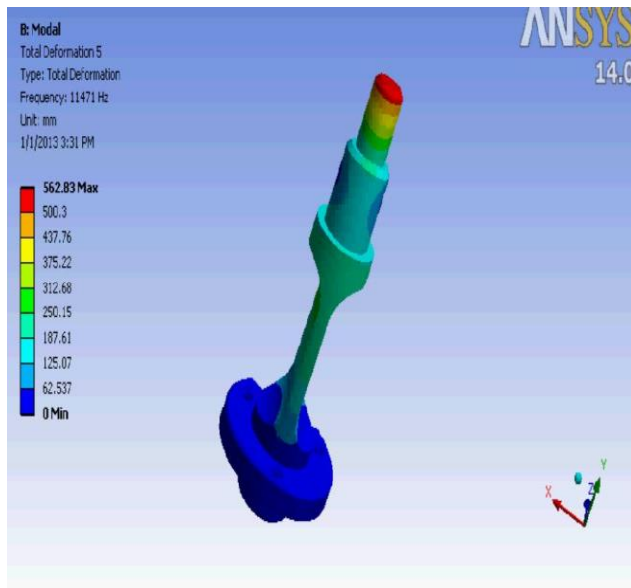


Figure 7: Fifth mode natural frequency and mode shape

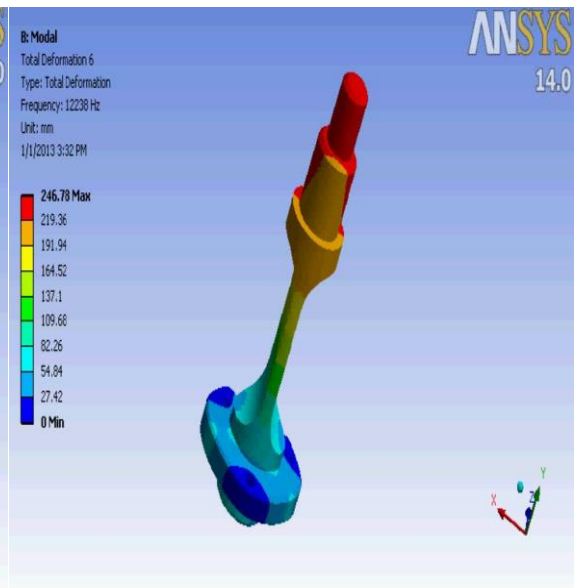


Figure 8: Sixth mode natural frequency and mode shape

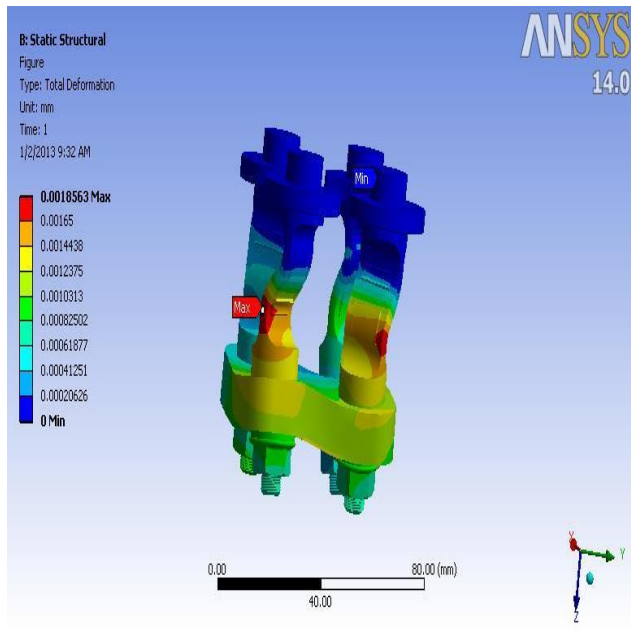


Figure 9: Displacement-Nodal Magnitude

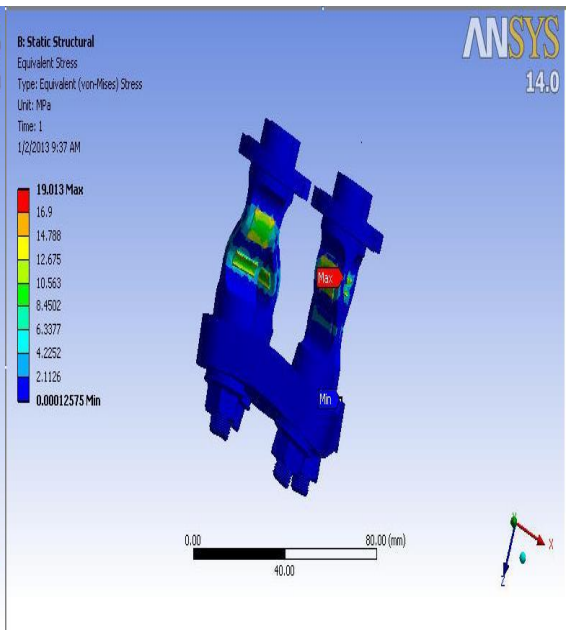


Figure 10: Stress-Element Nodal Von-Mises

IV. RESULTS AND DISCUSSION

Table1.Modal analysis results

| | |
|------------------|--------------------------|
| Software Used: | ANSYS14.0WORK BENCH |
| Solver: | Structures P.E. |
| Analysis Type: | Structural |
| Solution Type: | Modal |
| Linearity: | Linear |
| Time dependency: | Steady-state |
| Constraint set | 3CSK holes fixed all DOF |

| Results: | Frequency |
|----------|-----------|
| Mode1: | 525.6 Hz |
| Mode2: | 2016.4 Hz |
| Mode3: | 4001.7 Hz |
| Mode4: | 4904.6 Hz |
| Mode5: | 11471 Hz |
| Mode6: | 12238 Hz |

Table2: Material property data

| Material name | Material Type | Property | Value |
|---------------------------|---------------|-----------------|---------------------------------|
| Tin free Beryllium Bronze | Isotropic | Mass Density | 8.175e-006(kg/mm ³) |
| | | Young's Modulus | 120000000(mN/mm ²) |
| | | Poisson's Ratio | 0.3 |

4.1 Dither deflection under static load condition

Table3: Dither deflection under static load condition Solution Summary

| | |
|--|-----------------------------------|
| Solver: | Structures P.E. |
| Analysis Type: | Structural |
| Solution Type: | Linear Static's- Multi Constraint |
| Linearity: | Linear |
| Time dependency: | Steady-state |
| Loads (Piezoplategeneratedforces;Figure10) | 210N |
| Constraints | 12CSKholesfixedonfourTorsionbars |

Material Summary

| Material Name | Material Type | Property | |
|---------------------------|---------------|-----------------|---------------------------------|
| Tin free Beryllium Bronze | Isotropic | Mass Density | 8.175e-006(kg/mm ³) |
| | | Young's Modulus | 120000000 MPa |
| | | Poisson's Ratio | 0.3(Unitless) |

Results Summary:

Number of Steps in the Scenario Results=1

| Step Name | Displacement | Magnitude | Direction X | Direction Y | Direction Z |
|------------------------------|--------------|------------------|-------------------|------------------|------------------|
| Sub case Loads, Constrain1 | Maximum | 1.8563e-003 mm | 1.2638e-003mm | 1.9462e-04mm | 4.920.31e-004 mm |
| | Minimum | 0 mm | -1.1341e-03mm | -1.4285e-03mm | -6.1775e-04mm |
| Step Name | Stress | Von Mises | Maximum principle | Maximum shear | |
| Sub case-Loads, Constraints1 | Maximum | 19.013 MPa | 20.073 MPa | 10.149 MPa | |
| | Minimum | 1.2575 e-004 MPa | -1.3276 MPa | 7.2219 e-005 MPa | |

V. CONCLUSION

The Dither mechanism is very compact and provides continuous small rotation rate. The dither rotation rate can be varied by varying the voltage applied on the piezo plates. FEA can be used for designing a complicated torsion bar of nonuniform cross section for different applications.

Scope of Future Work:

We plan to test a new set of four super mirrors. In the same time the cavity will be shrunk slightly, from a side length of 1.40m to 1.35m (to account for radius of curvature of the new mirrors). The new mirrors will be of better quality—with less backscattering—than the current ones, improving the performance of the system. In the end, two ideas are intriguing us: the first is the purchase of a second piezoelectric transducer that could open new possibility. The second is more radical: the change to a passive ring cavity, with a laser externally injected. This should overcome any trouble with backscattering, since of course is a very different system.

REFERENCES

- [1]. Hutchings TJ 1978 Scale Factor non-linearity of a body dither laser gyro Proc. IEEE Nat'l Aerospace and electronic Conf. pp 549-55
- [2]. Shackleton BR 1987. Mechanical design considerations for a ring laser gyroscope dither mechanism Proc. Int. Conf. Mechanical technology of Inertial Devices (Newcastle, UK), (London :Institution of mechanical engineers) pp 105-12
- [3]. Kline-Schoder RJ and Wright MJ 1992 Design of a dither mirror control system mechanics
- [4]. Strength of materials by Ramamrutham,
- [5]. Theory of Machines by R.K.Jain
- [6]. Dr. Frederick Aronowitz, "Fundamentals of the Ring Laser Gyro", 11430, Manzanita Trail, Dewey, Az 86327, U.S.A.
- [7]. M. Faucheux, D. Fayoux and J. J. Roland, "The Ring Laser Gyro", Optics (Paris), 1988, Vol. 19, No 3, Pp. 101-115.
- [8]. Jeng Nan Juang and R. Radharamanan, "Evaluation of Ring Laser and Fiber Optic Gyroscope Technology", School Of Engineering, Mercer University, Macon, GA 31207 USA.
- [9]. F Aronowitz, "THE LASER GYRO," in Laser Applications, M. Ross Ed, (Academic, New York, 1971), pp 133-200.
- [10]. Wnag kedong, GU Qitai "KEY PROBLEM OF MECHANICALLY DITHERED SYSTEM OF RLG" ISSN 1007-0214 04/22 pp 304- 309, Volume 6, Number 4 China.
- [11]. A. Ramachander Rao, G.laxminarayana, M.K.Gupta, I.M.Chhabra, C.Vishnuvardhan Reddy "Analysis and Optimization Of Electrodes For Improving The Performance of Ring Laser Gyro" Eissn:2319-1163 Pissn: 2321-7308.
- [12]. Dong-Chan Lee, Gun Moon, Jae-Cheul Lee "Mechanical Dither Design for Ring Laser Gyroscope" VOL. 16 NO. 4, 485-491, 2002.
- [13]. Ayswarya P R, Pournami S S, Ravi Nambiar, "A Survey on Ring Laser Gyroscope Technology" International journal of computer applications(0975-8887), Volume 116- No.2, April 2015.

SAMPLE AUTHORS BIOGRAPHY

Penumarthi Chandra Sekhar Kumar was born in Vijayawada, India, in 1991. He received the Bachelor of Technology, Mechanical degree from the University of JNTU Kakinada, Vignans Engineering College, Vadlamudi, in the year of 2012, he is pursuing Master degree in Thermal Engineering in Kallam Hrinathreddy institute of technology from university JNTUK. His interests are doing a research in design side.



HARATAM ANIL KUMAR was born in Srikakulam, Andhra Pradesh, India, in 1988. He received the Bachelor in Aeronautical Engineering degree from the University of JNTU UNIVERSITY, KAKINADA, in 2013 and the Master in Naval Architecture and Marine Engineering degree from the University of Andhra University in 2015. His research interests include in ship structures, CFD and Hydrodynamics.



Marella Sai Chandra was born in Guntur, India, in 1991. He received the Bachelor of Technology degree from the JNTU Kakinada, in the year 2012, Masters Degree (M.Tech) from the JNTU Kakinada, in the year 2016, both in Mechanical Engineering. His research activities are doing the CFD and Design of Machine Components.

