

## FUZZY LOGIC CONTROLLED CASCADED SEPIC - QRC FED DC DRIVE SYSTEM WITH IMPROVED DYNAMIC RESPONSE

S. Vijaya Kumar<sup>1</sup>, S. Siva Nagaraju<sup>2</sup> and B. Stephen Charles<sup>3</sup>

<sup>1</sup>Research Scholar JNTUA, Ananthapur, Andhra Pradesh, India

<sup>2</sup>Professor, Dept. of EEE, JNTUK, Kakinada, Andhra Pradesh, India

<sup>3</sup>Principal, SSCET, Kurnool, Andhra Pradesh, India

### ABSTRACT

The objective of this work is to improve the dynamic response using FLC. This paper deals with design, modeling and simulation of closed loop cascaded SEPIC - QRC fed DC drive system. The closed loop SEPIC - QRC System is simulated with PI and FL controllers and their results are compared in terms of settling time and steady state error. The Fuzzy Logic Controlled cascaded SEPIC - QRC System is proposed in the present work to control the speed of the DC drive. The proposed system has advantage like high efficiency, low EMI and low switching losses.

**KEYWORDS:** Single – Ended Primary – Inductor Convertor (SEPIC), Quasi resonant Convertor (QRC), Zero current switching (ZCS), Pulse width modulation (PWM), Fuzzy Logic Control (FLC), EMI-Electro Magnetic Interference, PI - Proportional Integrator and SEPICQRCFDD- SEPIC-QRC fed DC Drive.

### I. INTRODUCTION

The single-ended primary inductor converter acts as a buck–boost DC–DC converter, where it changes its output voltage according to its duty cycle. Among known converters, the SEPIC, conventional buck–boost, and Cuk converters have the ability to step up and step down the input voltage. Hence, this converter can transfer energy for all irradiation levels. Another desirable feature is continuous output current, which allows converter output parallel connection, or conversion to a voltage source with minimal capacitance. The buck or boost converters are not preferable, due to the lack of output voltage flexibility. The SEPIC is chosen because the output voltage can be higher or lower than the input voltage. Also the input and output voltages are DC isolated.

Block diagram of the existing system shown in Figure.1. Fixed DC is converted into variable DC using QRC. The output of QRC is applied to the DC motor.

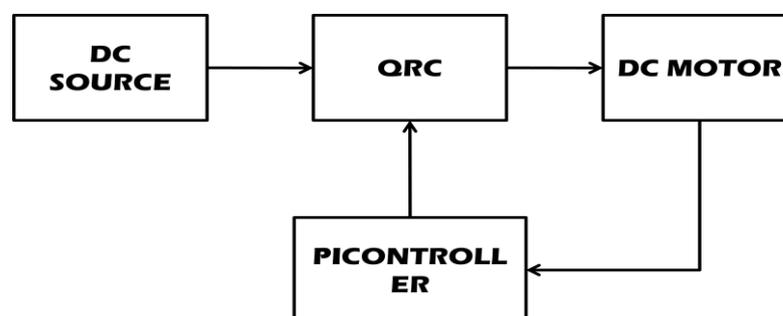
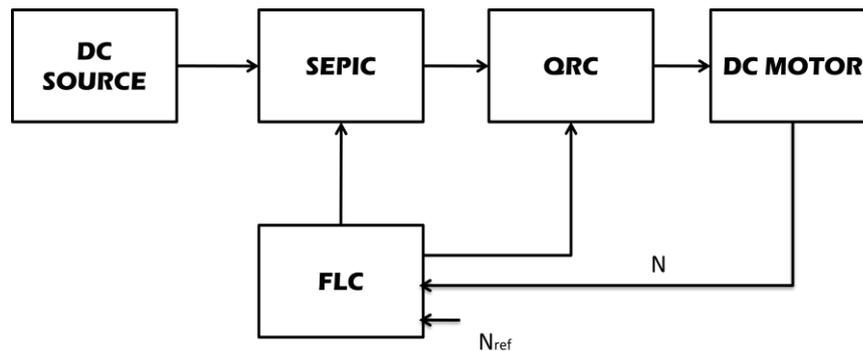


Figure 1. Block Diagram of the Existing System

The block diagram of SEPICQRCFDD is shown in Figure 2. The QRC is replaced by cascaded SEPIC- QRC based converter.



**Figure 2.** Block Diagram of the SEPICQRCFDD System

SEPICs are useful in applications in which a battery voltage can be above and below that of the regulator's intended output. Section 2 deals with literature survey. The analysis of SEPIC is presented in the section 3. The simulation results are given in section 4. The work is concluded in section 5 and the scope for future work is given in section 6

## II. LITERATURE SURVEY

Bridgeless Single-ended Primary Inductance Converter with improved power quality for welding power supplies is given by Narula.S and Singh.B.(2014). Design considerations of a multiple-input isolated single ended primary inductor converter for distributed generation sources is described by Sheng-Yang Yu, Ruichen Zhao and Kwasinski. A. (2011). Multi-loop controller for wide operating range single-ended primary inductor DC/DC converter said by Tsang. K.M. and Chan. W.L.(2011). Single Ended Primary Inductor Converter reliance of efficiency on switching frequency for use in MPPT application developed by Burmester. D, Rayudu. R and Exley.T.(2011). Maximum power point tracking of single-ended primary-inductor converter employing a novel optimisation technique for proportional-integral-derivative controller given by El Khateb. A, Rahim. N.A, Selvaraj. J and Uddin. M.N(2013). Multiple input single ended primary inductor converter for distributed generation applications given by Ruichen Zhao and Kwasinski. A. (2009). A Four-Switch Three-Phase SEPIC-Based Inverter Explained by Diab.M.S, Elserougi. A, Massoud. A.M, Abdel-Khalik. A.S and Ahmed. S. (2015). Fuzzy Logic Controller for MPPT SEPIC converter and PV single-phase inverter described by Khateb. A, Rahim, N.A and Selvaraj. J.(2011). High frequency quasi resonant SEPIC converter for wide range of operation explained by Unnikrishnan.C. and Raj. C.R.(2014). Performance of a DC motor fed from series and parallel quasi-resonant converters" developed by S.Rama Reddy and C. Chellamuthu,(1997). A Simple Large signal nonlinear modeling approach for fast simulation of Zero current switching Quasi resonant converters described by .L.K. Wong, Frank H. Leung and Peter K.S. Tam,(1997).

The above literature does not deal with SEPIC-QRC controlled DC drive. This work proposes cascaded SEPIC-QRC for the control of DC drive. The comparison of dynamic responses with PI and FLC is not reported in the literature.

## III. ANALYSIS

The SEPIC is allowing the electrical voltage at its output to be greater than, less than, or equal to that at its input. The output of the SEPIC is controlled by the duty cycle of the control transistor. A SEPIC is essentially a boost converter followed by a buck-boost converter, therefore it is similar to a traditional buck-boost converter, but has advantages of having non-inverted output, using a series capacitor to couple energy from the input to the output, and being capable of true shutdown when the switch is turned off, its output drops to 0 V, following a fairly hefty transient dump of charge.

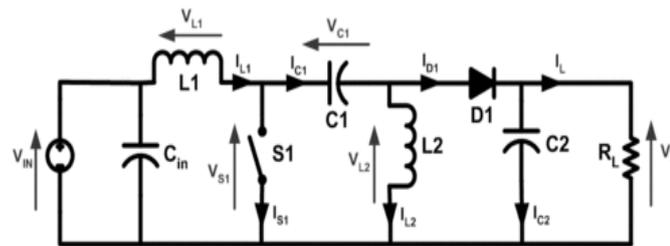


Figure 3. Schematic of SEPIC.

The schematic diagram for a basic SEPIC is shown in Figure 3. As with other switched mode power supplies, the SEPIC exchanges energy between the capacitors and inductors in order to convert from one voltage to another. The amount of energy exchanged is controlled by switch  $S_1$ , which is typically a transistor such as a MOSFET. MOSFETs offer much higher input impedance and lower voltage drop than bipolar junction transistors (BJTs), and do not require biasing resistors as MOSFET switching is controlled by differences in voltage rather than a current, as with BJTs.

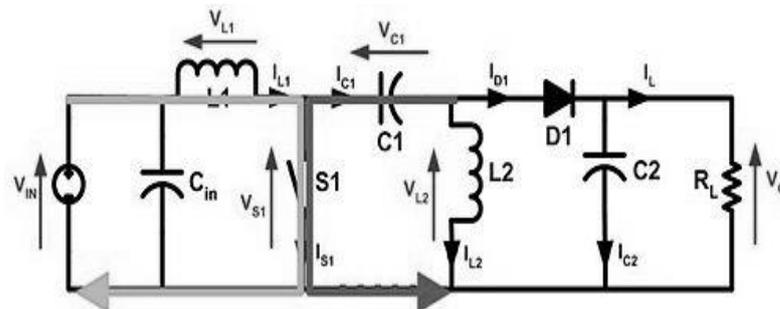


Figure 4. Circuit with  $S_1$  closed

A SEPIC is said to be in continuous-conduction mode if the current through the inductor  $L_1$  never falls to zero. During a SEPIC's steady-state operation, the average voltage across capacitor  $C_1$  ( $V_{C1}$ ) is equal to the input voltage ( $V_{in}$ ). Because capacitor  $C_1$  blocks direct current, the average current through it ( $I_{C1}$ ) is zero, making inductor  $L_2$  the only source of DC load current. Therefore, the average current through inductor  $L_2$  ( $I_{L2}$ ) is the same as the average load current and hence independent of the input voltage. Looking at average voltages, the following can be written:

$$V_{IN} = V_{L1} + V_{C1} + V_{L2} \text{ ----- (1)}$$

Because the average voltage of  $V_{C1}$  is equal to  $V_{IN}$ ,  $V_{L1} = -V_{L2}$ . For this reason, the two inductors can be wound on the same core. Since the voltages are the same in magnitude, their effects of the mutual inductance will be zero, assuming the polarity of the windings is correct. Also, since the voltages are the same in magnitude, the ripple currents from the two inductors will be equal in magnitude. The average currents can be summed as follows

$$I_{D1} = I_{L1} - I_{L2} \text{ ----- (2)}$$

When switch  $S_1$  is turned on, current  $I_{L1}$  increases and the current  $I_{L2}$  goes more negative. The energy to increase the current  $I_{L1}$  comes from the input source. Since  $S_1$  is a short when closed, and the instantaneous voltage  $V_{C1}$  is approximately  $V_{IN}$ , the voltage  $V_{L2}$  is approximately  $-V_{IN}$ . Therefore, the capacitor  $C_1$  supplies the energy to increase the magnitude of the current  $I_{L2}$  and thus increase the energy stored in  $L_2$ . The easiest way to visualize this is to consider the bias voltages of the circuit in a DC state, and then close  $S_1$ .

When switch  $S_1$  is turned off, the current  $I_{C1}$  becomes the same as the current  $I_{L1}$ , since inductors do not allow instantaneous changes in current. The current  $I_{L2}$  will continue in the negative direction, in fact it never reverse its direction. It can be seen from the diagram that a negative  $I_{L2}$  will add to the current  $I_{L1}$  to increase the current delivered to the load. Using Kirchhoff's Current Law, it can be shown that

$$I_{D1} = I_{C1} - I_{L2}. \text{ ----- (3)}$$

It can then be concluded, that while  $S_1$  is off, power is delivered to the load from both  $L_2$  and  $L_1$ .  $C_1$ , however is being charged by  $L_1$  during this off cycle, and will in turn recharge  $L_2$  during the on cycle.

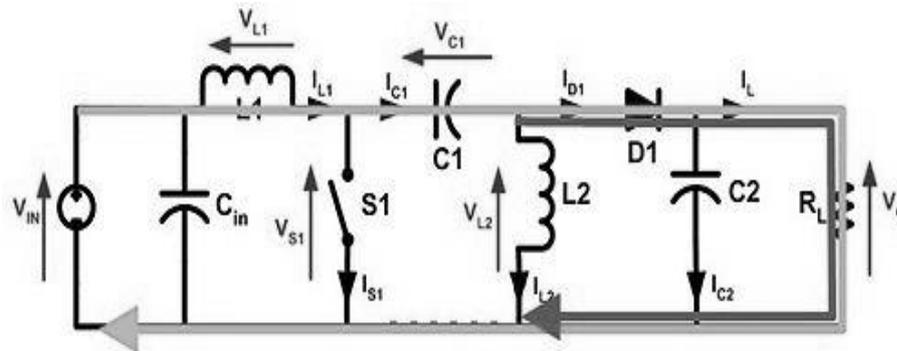


Figure 5. Circuit with S1 open

Because the voltage across capacitor  $C_1$  may reverse its direction every cycle, a non-polarized capacitor should be used. However, a polarized tantalum or electrolytic capacitor may be used in some cases, because the potential across capacitor  $C_1$  will not change unless the switch is closed long enough for a half cycle of resonance with inductor  $L_2$ , and by this time the current in inductor  $L_1$  could be quite large.

The capacitor  $C_{IN}$  is required to reduce the effects of the parasitic inductance and internal resistance of the power supply. The boost/buck capabilities of the SEPIC are possible because of capacitor  $C_1$  and inductor  $L_2$ . Inductor  $L_1$  and switch  $S_1$  create a standard boost converter, which generates a voltage ( $V_{S1}$ ) that is higher than  $V_{IN}$ , whose magnitude is determined by the duty cycle of the switch  $S_1$ . Since the average voltage across  $C_1$  is  $V_{IN}$ , the output voltage

$$V_O = V_{S1} - V_{IN}. \text{ ----- (4)}$$

If  $V_{S1}$  is less than double  $V_{IN}$ , then the output voltage will be less than the input voltage. If  $V_{S1}$  is greater than double  $V_{IN}$ , then the output voltage will be greater than the input voltage.

The evolution of switched-power supplies can be seen by coupling the two inductors in a SEPIC converter together, which begins to resemble a Fly back converter, the most basic of the transformer-isolated SMPS topologies.

#### IV. SIMULATION RESULTS

The values of parameters used for simulation are given in Table1

Table1. Parameters of Proposed System

Name of the parameter	Value
$V_{in}$	75V
$L_1$	8Mh
$L_2$	30mH
$C_{in}$	2000 $\mu$ F
$C_1$	0.30 $\mu$ F
$C_{bo}$	3000 $\mu$ F
MOSFET (IRF840)	500V/8A
DIODE	230V/1A
$V_0$	150V

The open loop controlled SEPIC-QRC fed DC drive system is shown in Figure 6. The step change in input voltage is shown in Figure 7. The input voltage increases from 70V to 80V at  $t=2$ Sec. The speed response is shown in Figure 8. The speed increases from 1700 rpm to 2000 rpm. The torque developed is shown in Figure 9. The torque settles at 14 N-m.

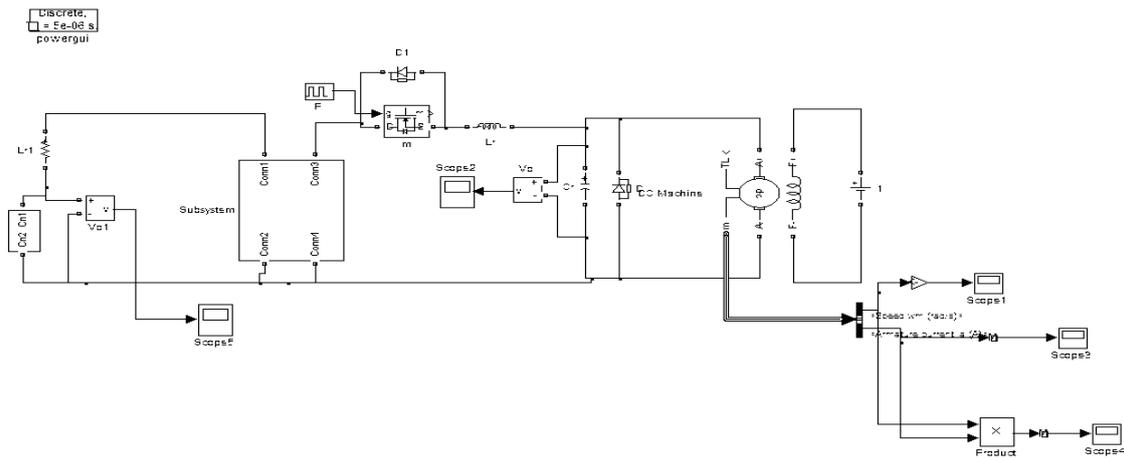


Figure 6. SEPIC-QRC Based Open Loop System

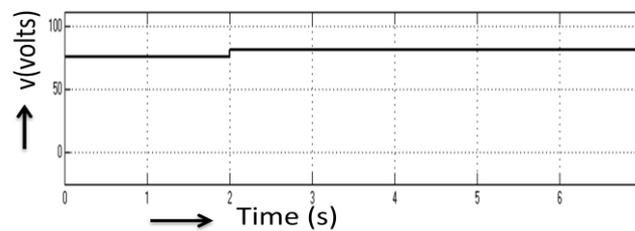


Figure 7. Input Voltage

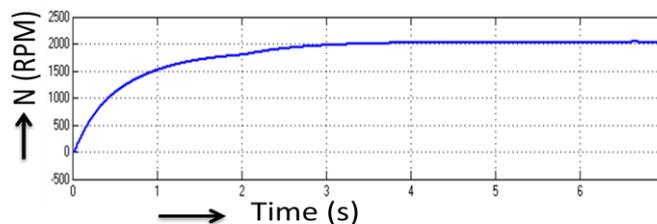


Figure 8. Motor Speed

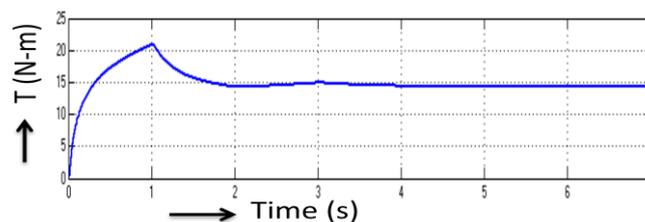


Figure 9. Motor Torque

Closed loop speed controlled system with PI controller is shown in Figure 10. The speed is sensed and it is compared with a reference speed of 1500 rpm. The error is applied to a PI controller and the output of the PI controller is applied to comparator. The comparator updates the pulse width of driving pulse given to the SEPIC converter. The step change in input voltage is shown in Figure 11. The speed response is shown in Figure 12. The speed oscillates and settles at the set reference value. The torque response is shown in Figure 13.

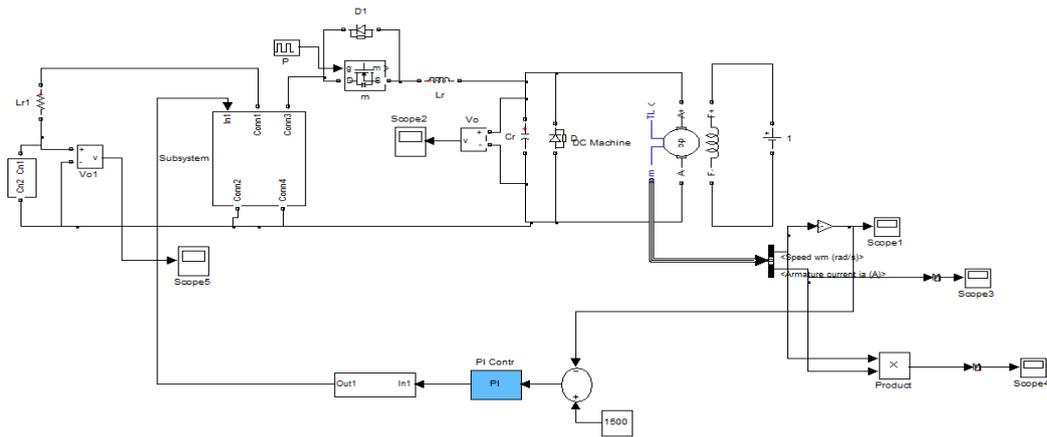


Figure 10. Closed Loop System with PI Controller

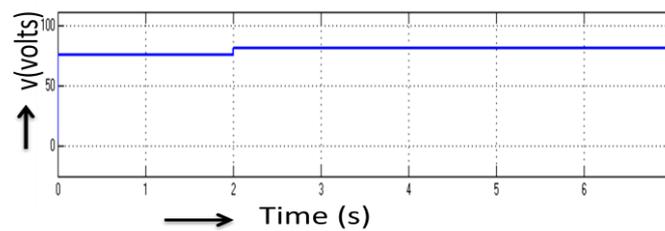


Figure 11. Input Voltage

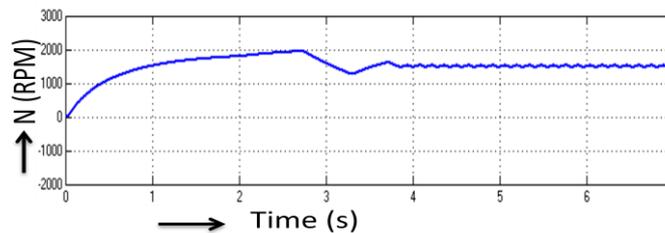


Figure 12. Motor Speed

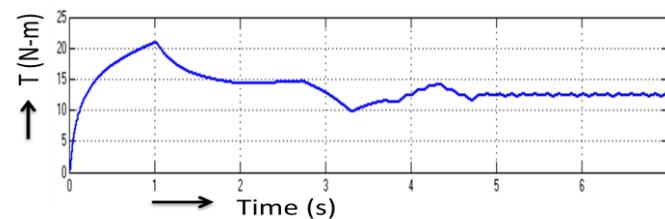


Figure 13. Motor Torque

Closed loop system with fuzzy controller is shown in Figure 14. The PI controller is replaced by a fuzzy logic controller. The inputs to FLC are error and its derivative. The step change in input voltage is shown in Figure 15. The speed response is shown in Figure 16. The speed reaches set value very smoothly. The response is shown in Figure 17. The summaries of time domain parameters are given in Table 2. It can be seen that settling time and steady state error are reduced by using FLC.

Table 2. Summary of responses with PI and Fuzzy Controllers

Controller	$t_r$	$t_s$	$t_p$	$E_{ss}$
PI Controller	1.3	4	2.8	2.5
Fuzzy	0.6	1.2	0	0.05

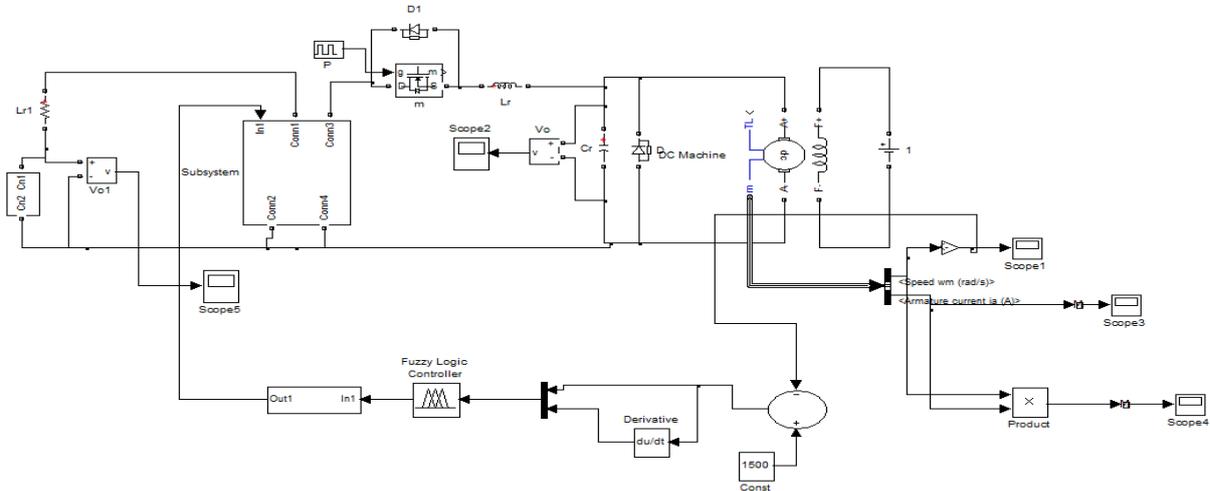


Figure 14. Closed Loop System with Fuzzy Controller

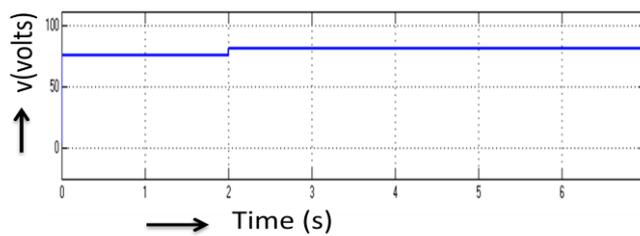


Figure 15. Input Voltage

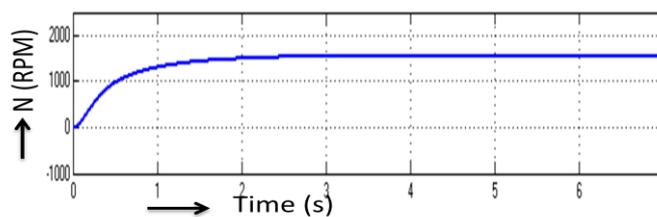


Figure 16. Motor Speed

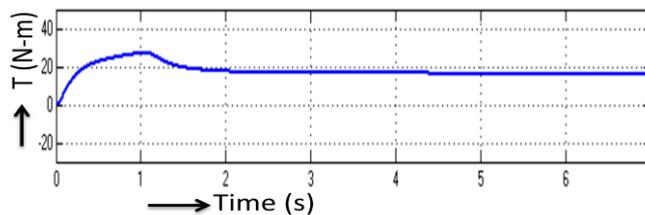


Figure 17. Motor Torque

## V. CONCLUSION

Closed loop PI and FLC based SEPIC –QRC fed DC drive systems are designed, modeled and simulated using Matlab successfully. Fuzzy logic controller is proposed in the present work to improve the dynamic response of the closed loop system. The proposed fuzzy logic controlled SEPIC-QRC drive system has improved dynamic response over PI controlled drive system. The disadvantage of the FLC is that it takes longer time for tuning.

## VI. FUTURE SCOPE

The Response of multi loop controlled drive system will be compared with FLC based drive system in future. The hardware will be implemented in future using PIC microcontroller for validating simulation results.

## REFERENCES

- [1]. Narula. S, Singh.B, & Bhuvaneswari.G, (2014) “ Bridgeless Single-ended Primary Inductance Converter with improved power quality for welding power supplies”Power Electronics (IICPE), IEEE 6th India International Conference.
- [2] Sheng-Yang Yu, Ruichen Zhao, & Kwasinski, A, (2011) “Design considerations of a multiple-input isolated single ended primary inductor converter (SEPIC) for distributed generation sources”Energy Conversion Congress and Exposition (ECCE), IEEE .
- [3]. Tsang, K.M. and Chan, W.L. (2011) "Multi-loop controller for wide operating range single-ended primary inductor DC/DC converter"Power Electronics, IET, Volume: 4, Issue: 8
- [4]. Burmester. D, Rayudu. R, & Exley.T., (2013) “Single Ended Primary Inductor Converter reliance of efficiency on switching frequency for use in MPPT application”Power and Energy Engineering Conference (APPEEC), IEEE PES Asia-Pacific.
- [5]. El Khateb. A, Rahim. N.A, Selvaraj. J, & Uddin. M.N,(2013) “Maximum power point tracking of single-ended primary-inductor converter employing a novel optimisation technique for proportional-integral-derivative controller”Power Electronics, IET, Volume: 6, Issue: 6
- [6]. Ruichen Zhao, & Kwasinski. A.(2009) “Multiple input single ended primary inductor converter (SEPIC) converter for distributed generation applications”Energy Conversion Congress and Exposition, ECCE , IEEE
- [7]. Diab. M.S, Elserougi. A. Massoud. A.M, Abdel-Khalik.A.S, & Ahmed. S, (2015) “A Four-Switch Three-Phase SEPIC-Based Inverter” Power Electronics, IEEE Transactions, Volume 30, Issue 9
- [8]. El Khateb. A, Rahim. N.A, & Selvaraj. J, (2011) “Fuzzy Logic Controller for MPPT SEPIC converter and PV single-phase inverter”Industrial Electronics and Applications (ISIEA), 2011 IEEE Symposium.
- [9]. Duran. E, Sidrach-de-Cardona. M, Galán. J, & Andujar. J.M.“Comparative analysis of buck-boost converters used to obtain I–V characteristic curves of photovoltaic modules”
- [10]. Jaschke. R, (2007) "Conduction Losses in DC/DC-Converters as buckboost/boostbuck synchronous rectifier types"Compatibility in Power Electronics, 2007. CPE '07
- [11]. Bhunia. M, Gupta. R, & Subudhi. B. (2014) “Cascaded DC-DC converter for a reliable standalone PV fed DC load”Power Electronics (IICPE), 2014 IEEE 6th India International Conference.
- [12]. Unnikrishnan.C.K,& Raj.C.R, (2014) “High frequency quasi resonant SEPIC converter for wide range of operation” Circuit, Power and Computing Technologies (ICCPCT), 2014 International Conference.
- [13]. S.Rama Reddy & C. Chellamuthu, (1997) “performance of a dc motor fed from series and parallel quasi-resonant converters”, International Journal of Power and Energy Systems, vo. 17, No. 3.
- [14]. L.K. Wong, Frank H. Leung and Peter KS. Tam, (May 1997) “A Simple Large signal nonlinear modeling approach for fast simulation of Zero current switching Quasi resonant converters” IEEE Transactions on power electronics, Vol. 12, no. 3.
- [15]. Bo-Tao lin and YimShu Lee (June 9-12, 1997). “Novel actively-clamped Zero current switching Quasi resibabt converters’ IEEE International symposium on circuits and systems, Hong Kong.

## AUTHORS

**S.Vijaya Kumar** was born in Kurnool, Andhra Pradesh, India, in 1974. He has Received B.Tech in Electrical and Electronics Engineering from Gandhi Institute of Technology and Management, VIZAG in 1999, and M.Tech in Computer Applications in Industrial Drives(CAID), in 2002. He is currently perusing Ph.D. Degree with the department of EEE from JNT University ATP. He is life member of ISTE. He is dedicated to teaching field from the last 13 years. His research areas Power electronics applications to Drives and power system.



**S. Sivanagaraju** was born in Kadapa, Andhra Pradesh, India, in 1970. has Received B.Tech in Electrical and Electronics Engineering from Gandhi Institute of Technology and Management, VIZAG in 1998, and M.Tech in Power System from IIT Karaghpur in 2000. He received his Ph.D Degree from JNT University ATP in 2004. At present he is working as Professor in JNTU Kakinada, East Godavari (district), Andhra Pradesh, India. His research interest includes Power distribution Automation and Power System operation and controls



**B. Stphen Charles** was born in Ongole, Andhra Pradesh, India, in 1965. He received his B.Tech degree in Electronics and Communication Engineering from Nagarjuna University, India in 1986. He received Ph.d degree in Electronics & Communication Engineering from Jawaharlal Nehru Technological University, Hyderabad in 2001. At present he is the Secretary, Correspondent and Principal in Stanley Stephen College of Engineering & Technology, Kurnool. Andhra Pradesh, India. His area of interest is Digital signal Processing.

